Particle Detectors for Colliders

Semiconductor Tracking Detectors

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Generic Detector

A detector cross-section, showing particle paths



Layers of Detector Systems around Collision Point

Solid State Detectors

- Specifically
 - microstrip & pixel trackers
- Have become trackers of choice (if affordable)
 - high spatial resolution
 - radiation hard
 - rely on development of micro-electronics fabrication techniques
- Central to heavy flavour tagging, lifetimes
 - vertex detection
 - B flavour
 - **Top**
 - Higgs



Top Quark Discovery at CDF



Semiconductors

• Have a large energy gap



Small number of charge carriers in conduction band
 electrons thermally excited across the band gap

$$n_i = AT^{\frac{3}{2}} \exp\left(\frac{-E_g}{2kT}\right)$$

 $n_i = 1.5 \times 10^{10} cm^{-3}$ in pure silicon at room temp increases with temperature

Doped Semiconductors



 In n-type, extra conduction electrons easily excited into conduction band

-increase conductivity

- In p-type, valence electrons excited into impurity band – holes in valence band conduct
 - n-type electrons majority carriers
 - p-type holes majority carriers







Depletion Zone as a Detector

- Reverse biased p-n junction no majority carriers no current
- Ionizing particle passing through depletion zone
- Liberates electron-hole pairs current flows
- Intrinsic field not high enough to efficiently collect carriers small signal
- Small depletion layer large capacitance large noise into electronics



Principle of micro-strip Detector



• 1 e-h pair / 3.6 eV - 10^2 e-h per micron - dense

• unlike gas – no multiplication of primary ionization 3×10^4 for 300μ

noise reduced by full depletion – reduce capacitance

Fabrication





Strip pattern of the microstrip detector



- position resolution < 10 microns
- limited by diffusion and delta-rays

Capacitive Charge - Division



Cross-section of the microstrip detector with capacitative charge division

• many strips resulting from 20μ pitch

→ many electronics channels – many \$\$

• stray capacitive coupling of strips – read out every n^{th} strip

 \Rightarrow read out every 6th strip – effective 120μ pitch – $\sigma: 8\mu$

Time Development of Signal













Figure 2

(*a*) Three-dimensional schematic of a single-sided, ac-coupled, polysilicon resistor-biased sensor showing the baseline of the CMS sensor at the LHC. During operation, the bias ring is connected to the GND (ground) potential, which is then distributed via the polysilicon bias resistors to the p^+ implant strips. The aluminum back plane is set to positive high voltage, depleting the full *n*-bulk volume of free-charge carriers by forming a pn-junction p^+ strip to n bulk. The long strips and thin decoupling oxide allow high coupling capacitances to be implanted directly into the sensor. The guard ring shapes the field at the borders. The n^{++} ring defines the active volume and prevents high field in the edge regions. (*b*) View of an actual sensor surface with a strip pitch of 80 μ m.



Temperature sensor





The ATLAS Inner Detector





SCT barrel



SCT EndCap











Fig. 9.4. (a) Geometry of a p-n junction. The static charge number density is n_D and n_A . The full depletion region is $d = A + D \sim A$. (b) Electric field for a p-n junction. (c) Electric potential for a p-n junction.

Signal from Si Detector

SAME TREATMENT AS SIGNAL IN GAS TUBE

• for a source charge $q_s \sim 5fC$

• peak electron (hole) currrent 710 nA (240 nA)

• How does this compare to the noise level?

electron mobility μ_e : 1400 cm²V⁻¹s⁻¹ drift velocity ~ 42 μ ns⁻¹ for 300 μ τ_D : 7 ns

 $I(t) = \frac{dQ}{dt} = \frac{\mu q_s E^2}{V_p}$

 $I(0) = \frac{2q_s}{\tau_D}$

 $I(\infty) = 0$

 $=\frac{4\mu q_{s}V_{B}}{d^{2}}\exp\left(-\frac{2t}{\tau_{D}}\right)$

 $=\frac{2q_{s}V_{B}}{\tau_{D}}\exp\left(-\frac{2t}{\tau_{D}}\right)$

 $\tau_D = \frac{d^2}{2\mu V_D} = \frac{d}{\mu E(0)}$



NOISE POWER IN A RESISTOR IS THERMAL ENERGY KT STREAD OVER ALL FREQ W

THERMAL NOISE
$$\rightarrow I_T$$

POWER
 $P = VI = I^2 R \rightarrow dI_7^2 = \frac{2k7}{R} \left(\frac{dw}{\pi}\right) - df$

SHOT NOISE $\rightarrow OUATIZED q AT ALL W$ $<math>dI_s^2 = q I \left(\frac{dw}{\pi}\right)$

$$R_B = k7/q_{z_{\overline{z}}} = l/q_m$$

Equivalent Circuit of Detector + Amplifier



Fig. 9.11. Amplifier and bandwidth limiting filter, $f(\omega)$ with source capacitance, C_s , source resistance, R_s , source charge, q_s , and input noise voltage, e_n .

- resistors source of thermal noise thermal energy kT
 - noise is spread uniformly over all frequencies

$$I_T \to P = VI_T = I_T^2 R$$
$$dI_T^2 = \frac{2kT}{R} \left(\frac{d\omega}{\pi}\right) \longleftarrow \text{ thermal noise}$$

current made of – discrete carriers

$$dI_s^2 = qI\left(\frac{d\omega}{\pi}\right)$$
 shot noise

need to limit bandwidth or infinite noise



$$\sqrt{qI} = 0.4 \, nA \, \sqrt{I \, Hz}$$
$$\sqrt{\frac{2kT}{R}} = 0.9 \, nA \, \sqrt{\frac{Hz}{R}}$$

- for a frequency range of 100 MHz and 1mA
- 126 nA pretty close to signal



Fig. 9.11. Amplifier and bandwidth limiting filter, $f(\omega)$ with source capacitance, C_s , source resistance, R_s , source charge, q_s , and input noise voltage, e_n .

- Thermal R_s
- Shot I_E
- Thermal R_B

$$d\overline{V}^{2} = d\overline{I}_{T}^{2}Z_{C_{S}}^{2} + d\overline{I}_{S}^{2}Z_{C_{S}}^{2} + d\overline{I}_{T}^{2}R_{B}^{2}$$

$$= \left[\frac{2kT}{R_{S}(\omega C_{S})^{2}} + \frac{qI_{B}}{(\omega C_{S})^{2}} + \frac{2kT}{g_{m}}\right] \left(\frac{d\omega}{\pi}\right)$$

$$\int_{1}^{1} \int_{0}^{1} \int_{0}^{0$$

After shaping (filter) Equivalent Noise Charge

$$ENCP = 2.72 \sqrt{\tau \left(\frac{kT}{2R_s} + q\frac{I_B}{4}\right)}$$
$$ENCS = 2.72C_s \sqrt{\frac{kT}{2g_m\tau}}$$

• Low temp • R_S large • I_B small • C_S small • R_B small • R_B small • series noise



RMS VOLTAGE

 $\langle v^2 \rangle = \int |f(w)|^2 \frac{dv^2}{dw} dw$ $= G^{2} \left[\left(\frac{k7}{2R} + \frac{q^{T}}{4} \right) \frac{T}{C_{s}^{2}} + \frac{k}{2q_{m}} \frac{T}{T} \right]$

FOR A SIGNAL CHARGE QS, IF THE FILTER

MATCHES THE FREQUENCY DISTRIBUTION OF THE SOURCE 2.72.

$$\begin{split} \begin{split} & \int S \xrightarrow{\longrightarrow} \int \frac{1}{C_s} \frac{G}{c_s} / e^{-t} = V \\ & CHARGE \quad ENC \xrightarrow{\longrightarrow} \left(ENC \cdot \frac{G}{C_s e} \right)^2 \equiv \langle V^2 \rangle \\ & A \\ &$$

P=> 11 RESISTOR ; S=> SERIES RESISTOR



- minimize detector cap minimize noise
- long strips? cheap too noisy



cf signal ~ 31000 electrons

Total Noise





Space Point

- Harder to fabricate (more expensive)
- Less material less MCS

Pixel Detector



R.S. Orr 2009 TRIUMF Summer Institute





Pixel System











"Ready for installation" date is 1st April 2007

Inner Detector (ID)



Utility of Si Tracker





Figure 6

The evolution of current and full depletion voltage ($\sim |N_{\text{eff}}|$) versus fluence and further annealing at room temperature (22). In panel *b*, the dip around 0.5×10^{14} in the fluence axis reveals the space charge sign inversion point; the minimum in the time axis illustrates when the reverse annealing becomes relevant.











- Order of magnitude increase in Data rates, Occupancy, Irradiation
- No TRT Si strips
- Pixels moved to larger radius
- New technology for inner layers
- R&D required on sensors, readout, and mechanical engineering

Pixel-layer Technologies



Figure 5: (a) Photograph of the ATLAS pixel diamond mounted in the carrier ready for bump bonding. (b) Zoom view of the pixel pattern after the under-bump metal is deposited.

- Harshest radiation environment (R~4cm)

 investigate new technologies
- 3D Si
- Thin silicon + 3D interconnects
- Gas over thin pixel (GOSSIP)
 - Diamond pixels
- May test in pre-SLHC b-layer replacement (~2012)