

# BIOT - SAVARD

## STEADY CURRENTS

STATIONARY CHARGES  $\rightarrow$   $\vec{E}$  CONSTANT, ELECTROSTATICS

STEADY CURRENTS  $\rightarrow$   $\vec{B}$  CONSTANT, MAGNETOSTATICS

$$\frac{\partial \rho}{\partial t} = 0 \quad ; \quad \frac{\partial \vec{J}}{\partial t} = \vec{0}$$

$\rightarrow$  OBVIOUSLY THIS IS AN IDEALIZATION  
CHARGE IS QUANTIZED IN POINTS  
SO, IN REALITY CURRENT ALWAYS  
VARIES  $\rightarrow$  WE CALL THIS  
"SHOT NOISE" IN ELECTRONICS

IN ELECTROSTATICS → STARTED FROM POINT CHARGES

↓ GENERALIZE

CHARGE DISTRIBUTIONS

MAGNETO STATICS → START FROM MOVING CHARGES

IN A WIRE  $|\vec{I}|$  MUST BE SAME EVERYWHERE

↳ CHARGE DOES NOT PILE UP SOMEWHERE

$$\vec{\nabla} \cdot \vec{J} = -\frac{\partial \rho}{\partial t} = 0$$

# MAGNETIC FIELD of A STEADY CURRENT BIOT-SAVARD

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{I} \times \hat{r}}{r^2} dl' = \frac{\mu_0}{4\pi} I \int \frac{dl' \times \hat{r}}{r^2}$$

NOTE  $r^2 \rightarrow$  SAME AS COULLOMB } ?  
GRAVITY }

INTEGRATION  $\rightarrow$  ALONG CURRENT PATH

$$\mu_0 = 4\pi \times 10^{-7} \frac{\text{NEWTONS}}{(\text{AMPERE})^2}$$

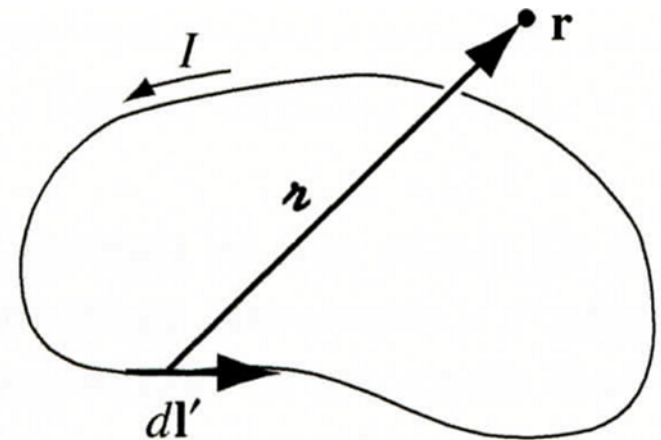
PERMEABILITY OF FREE SPACE

$\rightarrow$  EXACT NO.  $\rightarrow$  DEFINES A

$\vec{B}$  NEWTONS/AMPERE-METER

$\hookrightarrow$  TESLA

$$1 \text{ T} = 1 \text{ N/A}\cdot\text{m}$$



# MAGNETIC FIELD $S$ FROM LONG STRAIGHT WIRE CARRYING A STEADY CURRENT $I$

$d\vec{e}' \times \hat{r}$  POINTS OUT OF PAGE

$$|d\vec{e}' \times \hat{r}| = dl \sin \alpha = dl' \cos \theta$$

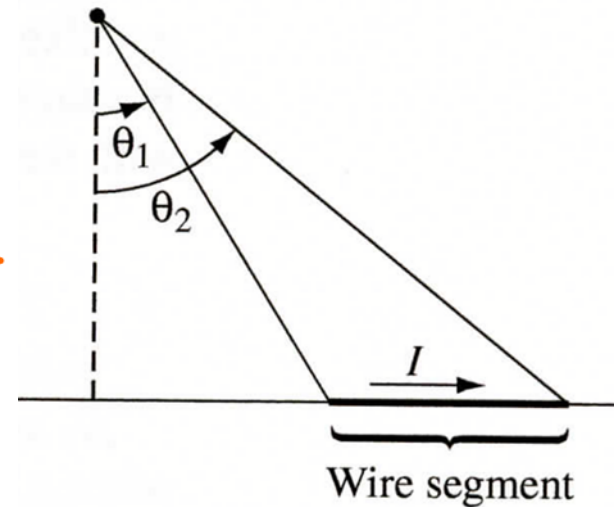
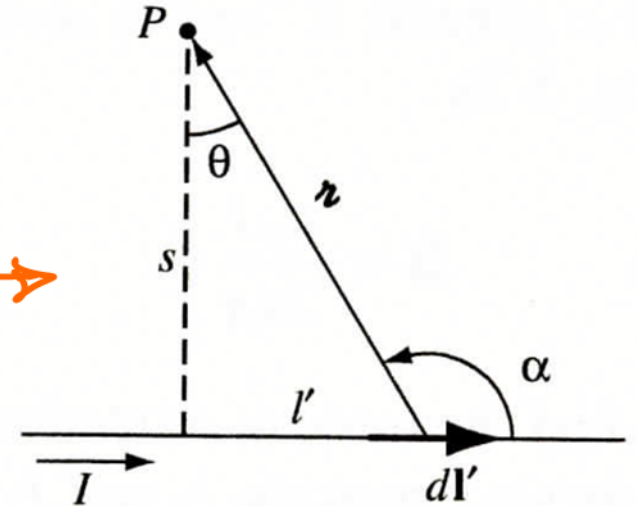
AND  $l' = S \tan \theta$

$$dl' = \frac{S}{\cos^2 \theta} d\theta$$

AND  $S = r \cos \theta \rightarrow \frac{1}{r^2} = \frac{\cos^2 \theta}{S^2}$

$$\vec{B} = \frac{\mu_0 I}{4\pi} \int_{\theta_1}^{\theta_2} \left( \frac{\cos^2 \theta}{S^2} \right) \left( \frac{S}{\cos^2 \theta} \right) \cos \theta d\theta$$

$$\vec{B} = \frac{\mu_0 I}{4\pi S} \int_{\theta_1}^{\theta_2} \cos \theta d\theta = \frac{\mu_0 I}{4\pi S} (\sin \theta_2 - \sin \theta_1)$$




$$\vec{B} = \frac{\mu_0 I}{4\pi r} \int_{\theta_1}^{\theta_2} \cos\theta d\theta = \frac{\mu_0 I}{4\pi r} (\sin\theta_2 - \sin\theta_1)$$

GIVES FIELD OF STRAIGHT SEGMENT

↳ CANNOT HAVE STEADY CURRENT

$$\int_{-\infty}^{+\infty} \longrightarrow \int_{-\pi/2}^{+\pi/2} d\theta$$

$$B = \frac{\mu_0 I}{2\pi r}$$


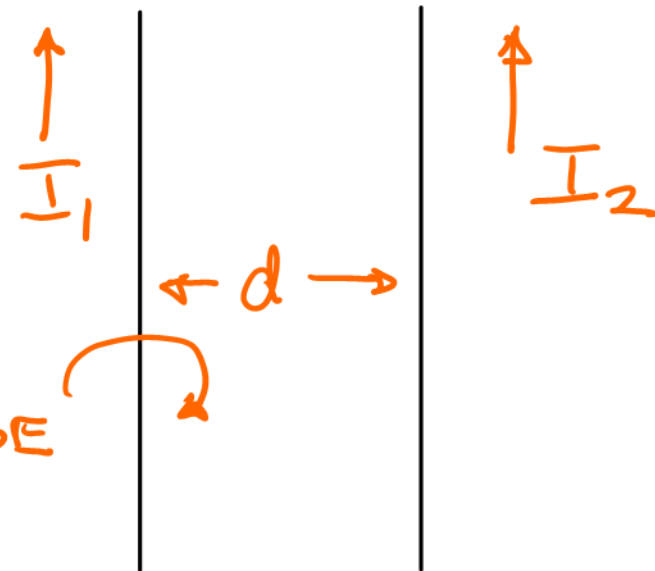
↳ DEPENDENCE SAME AS ELECTROSTATICS

$$\vec{B} = \frac{\mu_0 I}{2\pi r} \hat{\phi}$$

• FORCE BETWEEN TWO LONG STRAIGHT WIRES

• FIELD AT (2) DUE TO (1)

$$B = \frac{\mu_0 I_1}{2\pi d} \quad \text{INTO PAGE}$$



$$\vec{F}_{\text{MAG ON (2)}} = \int I_2 (d\vec{\ell} \times \vec{B}) d\ell = I_2 \left( \frac{\mu_0 I_1}{2\pi d} \right) \int_{-\infty}^{+\infty} d\ell$$

$$\text{FORCE / UNIT LENGTH} = \frac{\mu_0}{2\pi} \frac{I_1 I_2}{d}$$

$I_1 \uparrow \quad \downarrow \quad I_2 \quad \rightarrow \text{REPULSIVE}$

$I_1 \uparrow \quad \uparrow \quad I_2 \quad \rightarrow \text{ATTRACTIVE}$

MAGNETIC FIELD  $z$  ABOVE CENTER of  
 CIRCULAR LOOP R CURRENT I

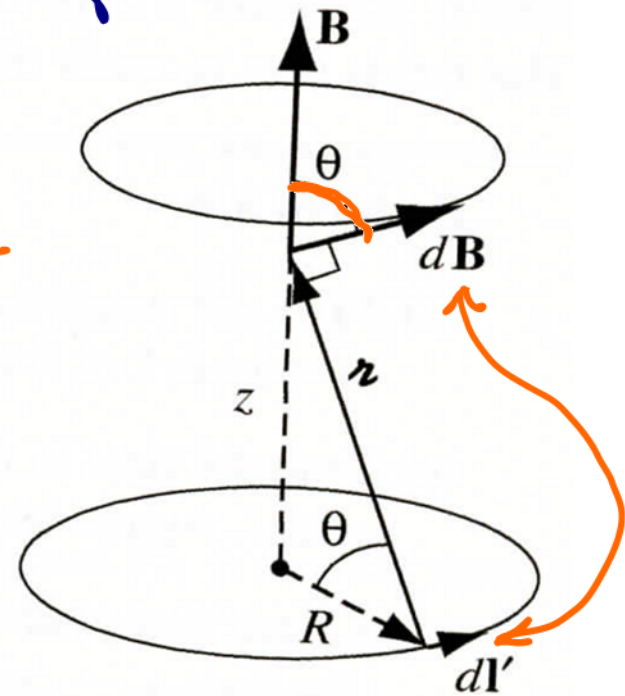
$d\vec{B}$  DUE TO  $dI'$  NOT HORIZONTAL

$\int \rightarrow$  SWEEPS OUT A CONE

HORIZONTAL COMPONENTS CANCEL

VERTICAL  $B(z) = \frac{\mu_0 I}{4\pi} \int \frac{dl'}{r^2} \cos\theta$

$\underbrace{\hspace{10em}}_{dl', r^2 \text{ PERP}}$



$\cos\theta, r^2$  ARE CONSTANT  $\int dl' = 2\pi R$

$$B(z) = \frac{\mu_0 I}{4\pi} \left( \frac{\cos\theta}{r^2} \right) 2\pi R = \frac{\mu_0 I}{2} \frac{R^2}{(R^2 + z^2)^{3/2}}$$

# BIOT-SAVARD

→ SURFACE & VOLUME

SURFACE  $\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{K}(\vec{r}') \times \hat{r}}{r^2} da'$

VOLUME  $\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{J}(\vec{r}') \times \hat{r}}{r^2} d\tau'$

MOVING CHARGE?  $\frac{\mu_0}{4\pi} q \frac{\vec{v} \times \hat{r}}{r^2}$

WRONG → MOVING CHARGE IS NOT A STEADY CURRENT

SUPERPOSITION APPLIES TO  $\vec{B}$

JUST LIKE  $\vec{E}$



# DIVERGENCE & CURL OF $\vec{B}$

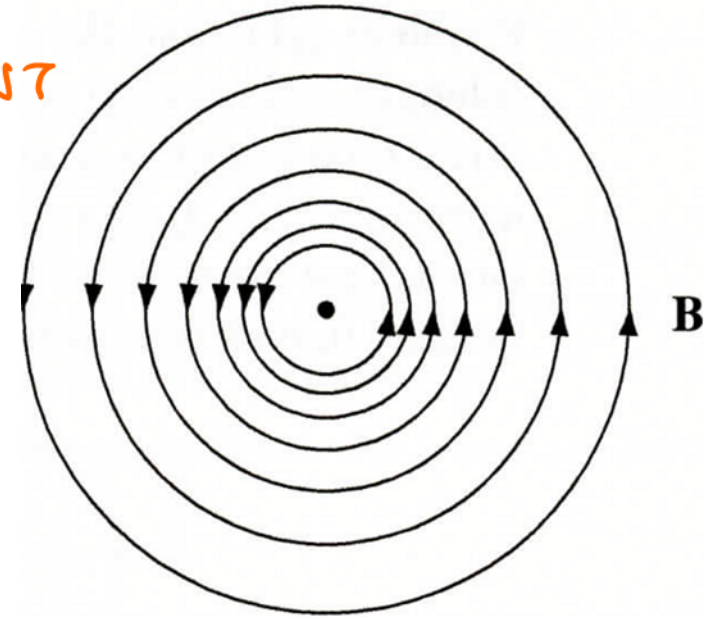
## STRAIGHT LINE CURRENTS

INFINITE STRAIGHT WIRE

MUST HAVE  $\vec{\nabla} \times \vec{B} \neq 0$  →

USE CIRCULAR PATH RADIUS 'S'  
CENTRED ON WIRE

CURRENT  
OUT  
OF  
PAGE



$$\oint \vec{B} \cdot d\vec{\ell} = \oint \frac{\mu_0 I}{2\pi s} d\ell = \frac{\mu_0 I}{2\pi s} \oint d\ell = \mu_0 I$$

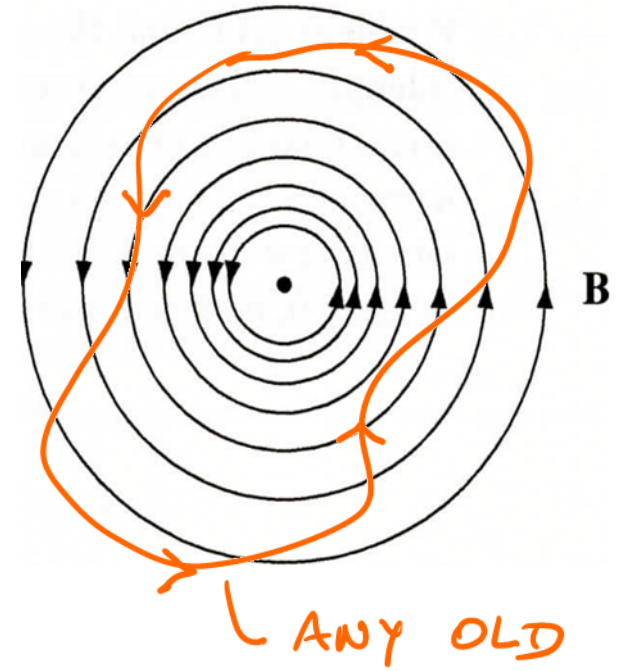
$\oint$  INDEPENDENT OF  $s \rightarrow \vec{B}$  DECREASES AT  
SAME RATE CIRCUMFERENCE  
INCREASES

COULD USE ANY CONTOUR FOR  $\oint$

SEE INDEPENDENCE of PATH  $\rightarrow$  CYLINDRICAL COORDS  
 $(s, \phi, z)$

$$\vec{B} = \left( \frac{\mu_0 I}{2\pi s} \right) \hat{\phi} ; \quad d\vec{\ell} = ds \hat{s} + s d\phi \hat{\phi} + dz \hat{z}$$

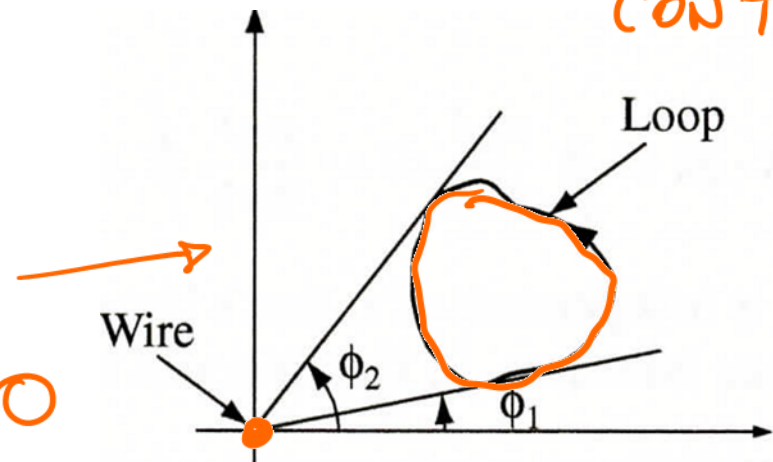
$$\begin{aligned} \oint \vec{B} \cdot d\vec{\ell} &= \frac{\mu_0 I}{2\pi} \oint \frac{1}{s} \cdot s d\phi \\ &= \frac{\mu_0 I}{2\pi} \int_0^{2\pi} d\phi \\ &= \mu_0 I \text{ AS BEFORE} \end{aligned}$$



CONTOUR ENCLOSES WIRE

AND  $\oint$  AROUND ONCE.

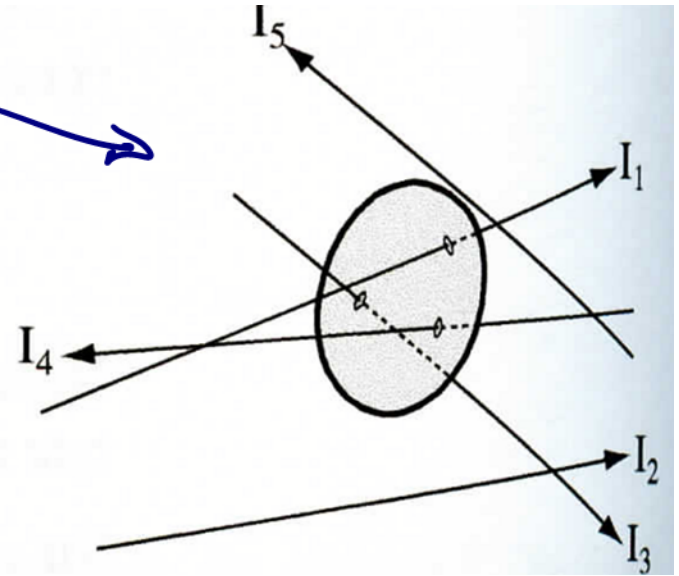
$$\int_{\phi_1}^{\phi_2} + \int_{\phi_2}^{\phi_1} = 0$$



BUNDLE of WIRES

EACH WIRE THAT PASSES THROUGH LOOP CONTRIBUTES

$$\mu_0 I$$



THOSE THAT DO NOT PASS THROUGH LOOP

CONTRIBUTE NOTHING

$$\oint \vec{B} \cdot d\vec{e} = \mu_0 I_{\text{ENCLOSED}}$$

$$I_{\text{ENCL}} = \int \vec{J} \cdot d\vec{a}$$

VOLUME CURRENT DENSITY

$$\int (\nabla \times \vec{B}) \cdot d\vec{a} = \mu_0 \int \vec{J} \cdot d\vec{a}$$

FROM STOKES

$$\nabla \times \vec{B} = \mu_0 \vec{J}$$

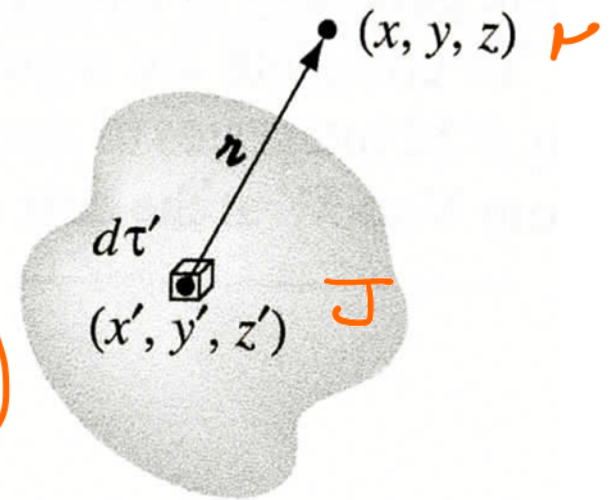
THIS ASSUMES A LONG STRAIGHT WIRE

→ DO IT GENERALLY ↓

# GENERAL DIVERGENCE & CURL of $\vec{B}$

BIOT & SAVARD for GENERAL VOLUME

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{J}(\vec{r}') \times \hat{r}}{r^2} d\tau'$$



$$\vec{B} \equiv \vec{B}(x, y, z); \quad \vec{J} \equiv \vec{J}(x', y', z')$$

$$\vec{r} = (x - x')\hat{x} + (y - y')\hat{y} + (z - z')\hat{z}$$

$$d\tau' = dx' dy' dz'$$

$\int$  IS OVER PRIMED COORDINATES

$\vec{\nabla} \times \vec{B} \rightarrow$  REFERS TO UNPRIMED COORDINATES

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{J}(\vec{r}') \times \hat{r}}{r^2} d\tau'$$

$$\vec{\nabla} \cdot \vec{B} = \frac{\mu_0}{4\pi} \int \vec{\nabla} \cdot \left( \vec{J} \times \frac{\hat{r}}{r^2} \right) d\tau'$$

GENERALLY  $\vec{\nabla} \cdot (\vec{A} \times \vec{B}) = \vec{B} \cdot (\vec{\nabla} \times \vec{A}) - \vec{A} \cdot (\vec{\nabla} \times \vec{B})$

$$\vec{\nabla} \cdot \left( \vec{J} \times \frac{\hat{r}}{r^2} \right) = \frac{\hat{r}}{r^2} \cdot (\vec{\nabla} \times \vec{J}) - \vec{J} \cdot \left( \vec{\nabla} \times \frac{\hat{r}}{r^2} \right)$$

ACTS ON  
UNPRIME COORDS

DOES NOT DEPEND ON  
UNPRIME COORDINATES

$$\vec{\nabla} \times \vec{J} = 0$$

$$\left( \vec{\nabla} \times \frac{\hat{r}}{r^2} \right) = \vec{0}$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

AGAIN → 
$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{J}(\vec{r}') \times \hat{e}_L}{r^2} d\tau'$$

$$\vec{\nabla} \times \vec{B} = \frac{\mu_0}{4\pi} \int \vec{\nabla} \times \left( \vec{J} \times \frac{\hat{e}_L}{r^2} \right) d\tau'$$

$$\vec{\nabla} \times (\vec{A} \times \vec{B}) = (\vec{B} \cdot \vec{\nabla}) \vec{A} - (\vec{A} \cdot \vec{\nabla}) \vec{B} + \vec{A} (\vec{\nabla} \cdot \vec{B}) - \vec{B} (\vec{\nabla} \cdot \vec{A})$$

$$\begin{aligned} \vec{\nabla} \times \left( \vec{J} \times \frac{\hat{e}_L}{r^2} \right) &= \left( \frac{\hat{e}_L}{r^2} \cdot \vec{\nabla} \right) \vec{J} - (\vec{J} \cdot \vec{\nabla}) \frac{\hat{e}_L}{r^2} + \vec{J} (\vec{\nabla} \cdot \frac{\hat{e}_L}{r^2}) \\ &\quad - \frac{\hat{e}_L}{r^2} (\vec{\nabla} \cdot \vec{J}) \end{aligned}$$

TERMS IN  $\vec{\nabla} \cdot \vec{J} \Rightarrow 0$  —  $\vec{J} \neq \vec{J}(x, y, z)$

$$\vec{\nabla} \times \left( \vec{J} \times \frac{\hat{e}_L}{r^2} \right) = \vec{J} (\vec{\nabla} \cdot \frac{\hat{e}_L}{r^2}) - (\vec{J} \cdot \vec{\nabla}) \frac{\hat{e}_L}{r^2}$$

$$\vec{\nabla} \cdot \left( \frac{\hat{e}_L}{r^2} \right) = 4\pi \delta^3(\vec{r}) \quad \uparrow$$

↳ MUST SHOW THIS IS ZERO

ASSUMING  $\int (\vec{J} \cdot \vec{\nabla}) \frac{e^{\hat{L}}}{r^2} \rightarrow 0$

$$\vec{\nabla} \times \vec{B} = \frac{\mu_0}{4\pi} \int \vec{\nabla} \times \left( \vec{J} \times \frac{e^{\hat{L}}}{r^2} \right) d\tau' = \int \vec{J} \left( \underbrace{\vec{\nabla} \cdot \frac{e^{\hat{L}}}{r^2}}_{\vec{\nabla} \cdot \left( \frac{e^{\hat{L}}}{r^2} \right) = 4\pi \delta^3(\vec{r})} \right) d\tau'$$

$$\vec{\nabla} \times \vec{B} = \frac{\mu_0}{4\pi} \int \vec{J}(\vec{r}') 4\pi \delta^3(\vec{r} - \vec{r}') d\tau'$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}(\vec{r}) + ?$$

WITHOUT ASSUMING  
STRAIGHT LINE CURRENT

STILL NEED TO  
SHOW THAT THIS = 0

$$-(\vec{J} \cdot \vec{\nabla}) \frac{\hat{z}}{r^2} = 0 \quad ???$$

$$\vec{r} = (x-x')\hat{x} + (y-y')\hat{y} - (z-z')\hat{z}$$

↑ DEPENDS DIFFERENCE OF COORDINATES

$$\frac{\partial}{\partial x} f(x-x') = -\frac{\partial}{\partial x'} f(x-x')$$

$$\vec{\nabla}(r-r') = -\vec{\nabla}'(r-r')$$

$$-(\vec{J} \cdot \vec{\nabla}) \frac{\hat{z}}{r^2} = (\vec{J} \cdot \vec{\nabla}') \frac{\hat{z}}{r^2}$$

LOOK AT  
x-COMPONENT

$$(\vec{J} \cdot \vec{\nabla}') \left( \frac{x-x'}{r^3} \right)$$



$$(\vec{J} \cdot \vec{\nabla}') \left( \frac{x-x'}{r_3} \right)$$

USE  $\vec{\nabla} \cdot (f\vec{A}) = f(\vec{\nabla} \cdot \vec{A}) + \vec{A} \cdot (\vec{\nabla} f)$

$$\vec{J} \cdot \vec{\nabla}' \left( \frac{x-x'}{r_3} \right) = \vec{\nabla}' \left( \frac{x-x'}{r_3} \right) \cdot \vec{J} - \left( \frac{x-x'}{r_3} \right) \vec{\nabla}' \cdot \vec{J}$$

$\vec{\nabla}' \cdot \vec{J} = 0$  FOR STEADY CURRENT

$$(\vec{J} \cdot \vec{\nabla}') \left( \frac{x-x'}{r_3} \right) = \vec{\nabla}' \left( \frac{x-x'}{r_3} \cdot \vec{J} \right)$$

$$- (\vec{J} \cdot \vec{\nabla}) \left( \frac{x-x'}{r_3} \right) = \vec{\nabla}' \left( \frac{x-x'}{r_3} \cdot \vec{J} \right)$$

LOOK MA  
NO PRIME

WANT TO  
SHOW = 0

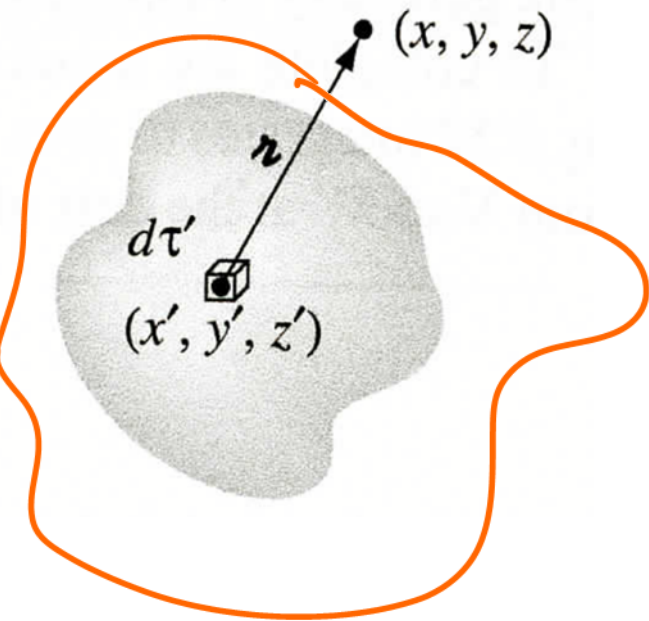
$\int$  THIS  $\rightarrow$  SEE IF  
IT IS ZERO

$$\int \vec{\nabla}' \left( \frac{1}{r} \right) \vec{J} d\tau' = \oint \left( \frac{1}{r} \right) \vec{J} \cdot d\vec{a}'$$

$\vec{J} = \vec{J}(x', y', z')$

DIVERGENCE  
THEOREM

$$\oint_S \left( \frac{1}{r} \right) \vec{J} \cdot d\vec{a}'$$



Ahh CURRENT DENSITY IS  
IN VOLUME

↳ SURFACE  $\int = 0$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}(\vec{r}) \quad \text{GENERALLY}$$