

# AMPERE'S LAW

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J} \quad \leftarrow \text{AMPERE'S LAW}$$

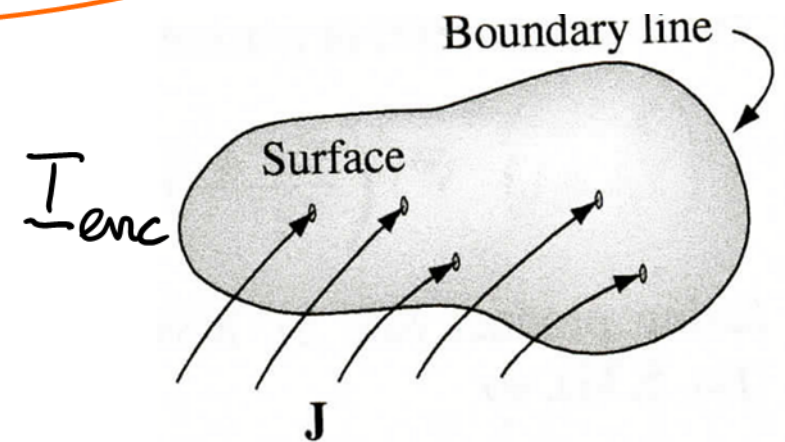
CAN CONVERT TO INTEGRAL FORM  $\rightarrow$  STOKES'

$$\int_S (\vec{\nabla} \times \vec{v}) \cdot d\vec{a} = \oint_P \vec{v} \cdot d\vec{e}$$

$$\int (\vec{\nabla} \times \vec{B}) \cdot d\vec{a} = \oint_P \vec{B} \cdot d\vec{e} = \mu_0 \int \vec{J} \cdot d\vec{a}$$

$$\int \vec{J} \cdot d\vec{a} \rightarrow \text{TOTAL CURRENT THRU SURFACE}$$

$$\oint \vec{B} \cdot d\vec{e} = \mu_0 I_{enc}$$



$$\oint \vec{B} \cdot d\vec{\ell} = \mu_0 I_{enc}$$

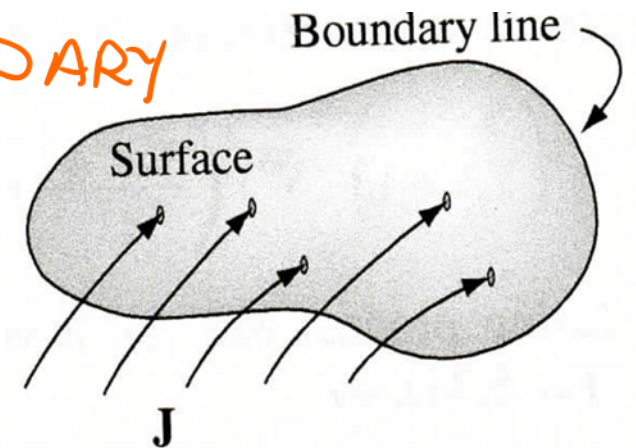
SHOWED THAT THIS WAS TRUE FOR STRAIGHT WIRE

HAVE GENERALIZED TO ARBITRARY CURRENT

WHICH WAY TO  $\oint$  AROUND LOOP?

APPLY RIGHT HAND RULE ON BOUNDARY

THUMB GIVES +VE CURRENT



ELECTROSTATICS: COULOMB  $\rightarrow$  GAUSS

MAGNETOSTATICS: BIOT - SAVARD  $\rightarrow$  AMPÈRE

USEFUL WHEN CURRENT  
HAS SOME SYMMETRY

EXAMPLE! FIND MAGNETIC FIELD DISTANCE  $s$  FROM  
LONG STRAIGHT WIRE CARRYING  $I$

DIRECTION OF  $\vec{B}$   $\rightarrow$  R.H. RULE

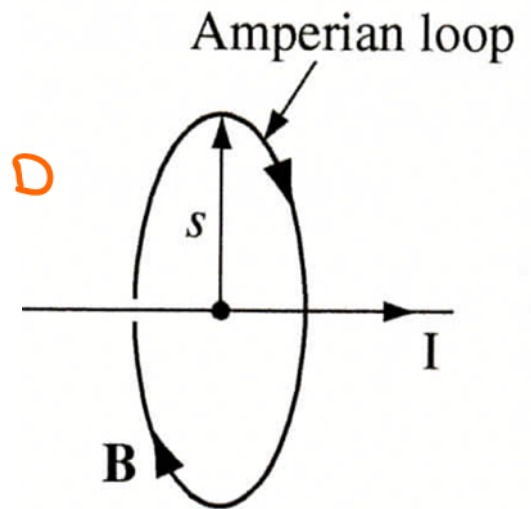
SYMMETRY  $\rightarrow$   $\vec{B}$  CONSTANT AROUND  
LOOP

$$\oint \vec{B} \cdot d\vec{\ell} = B \oint d\ell = B 2\pi s = \mu_0 I_{enc} \\ = \mu_0 I$$

$$B = \frac{\mu_0 I}{2\pi s}$$



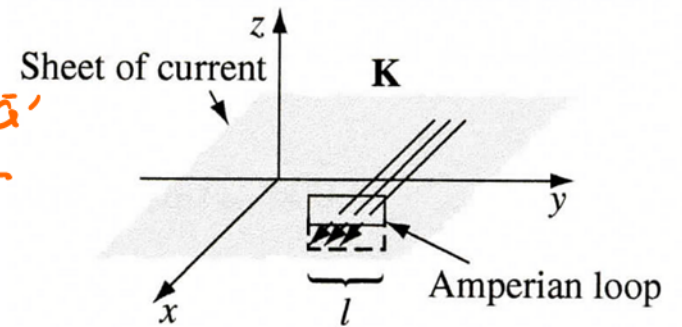
SAME AS BIOT-SAVARD  
BUT EASIER



EXAMPLE: FIND THE MAGNETIC FIELD OF AN INFINITE UNIFORM SURFACE CURRENT  
 $\vec{K} = K \hat{x}$  FLOWING OVER XY PLANE.

DIRECTION OF  $\vec{B}$

BIOT-SAVARD 
$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{K}(\vec{r}') \times \hat{r}}{r^2} da'$$



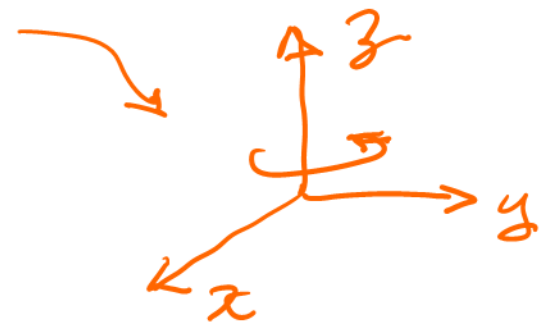
SO  $\vec{B}$  IS PERP TO CURRENT.  $\hookrightarrow$  NO x COMPONENT

z-COMPONENT — IF FIELD POINTED AWAY FROM PLANE  $\rightarrow$  REVERSING CURRENT

WOULD MAKE FIELD POINT INTO PLANE

z-COMPONENT CANNOT DEPEND ON DIRECTION OF CURRENT IN XY PLANE

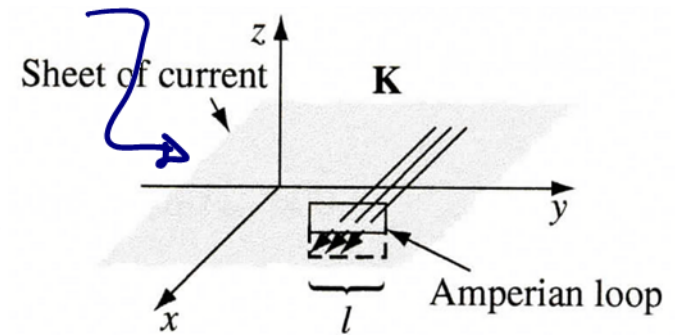
$\vec{B}$  ONLY HAS y-COMPONENT



# AMPERIAN LOOP IN PLANE

$$\oint \vec{B} \cdot d\vec{l} = 2Bl = \mu_0 I_{en} = \mu_0 Kl$$

$$B = \frac{\mu_0}{2} K$$



HEIGHT OF LOOP  $\rightarrow 0$

$$\vec{B} = \begin{cases} + (\mu_0/2) K \hat{y} & \text{for } z < 0 \\ - (\mu_0/2) K \hat{y} & \text{for } z > 0 \end{cases}$$

FIELD IS INDEPENDENT OF DISTANCE FROM PLANE

Cf  $\rightarrow$  ELECTROSTATIC CASE

EXAMPLE: MAGNETIC FIELD OF VERY LONG SOLENOID

$n$  CLOSELY WOUND TURNS PER UNIT LENGTH, ON A CYLINDER OF RADIUS  $R$ . EACH TURN CARRIES A STEADY CURRENT  $I$

CLOSELY WOUND TURNS  $\rightarrow$  EACH IS CIRCULAR

WHAT IS THE DIRECTION OF  $\vec{B}$

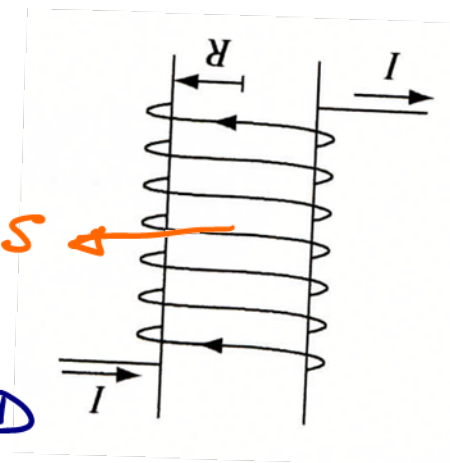
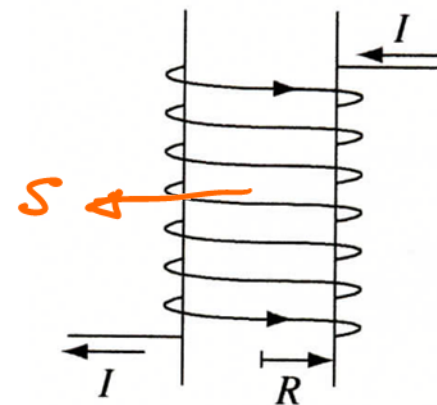
COULD IT HAVE A RADIAL COMPONENT?

- IF  $B_s$  +VE, REVERSING CURRENT  $\rightarrow B_s$  -VE

$\hookrightarrow$  EQUIVALENT TO TURNING THE

SOLENOID UPSIDE DOWN

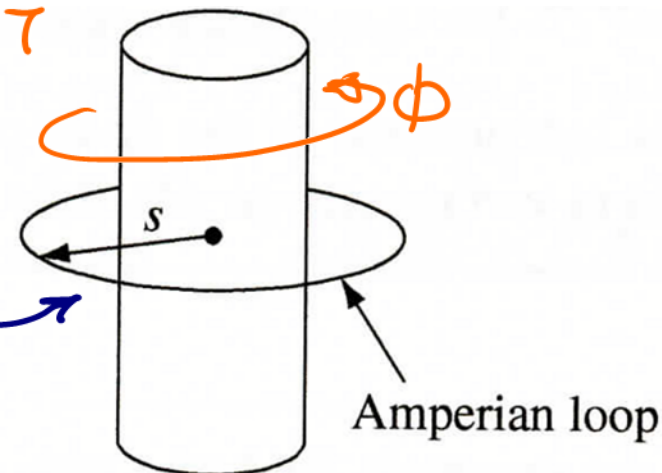
CAN'T CHANGE  
MAGNETIC FIELD



COULD THERE BE A  $\phi$  COMPONENT OF  $\vec{B}$ ?

$B_\phi$  WOULD BE CONSTANT AROUND

$$\oint \vec{B} \cdot d\vec{\ell} = B_\phi \cdot 2\pi s = \mu_0 I_{enc} = 0$$



- MAGNET FIELD  $\parallel$  to AXIS
- RH RULE  $\uparrow \vec{B}$  INSIDE  $\downarrow \vec{B}$  OUTSIDE
- GOES TO ZERO FAR FROM AXIS

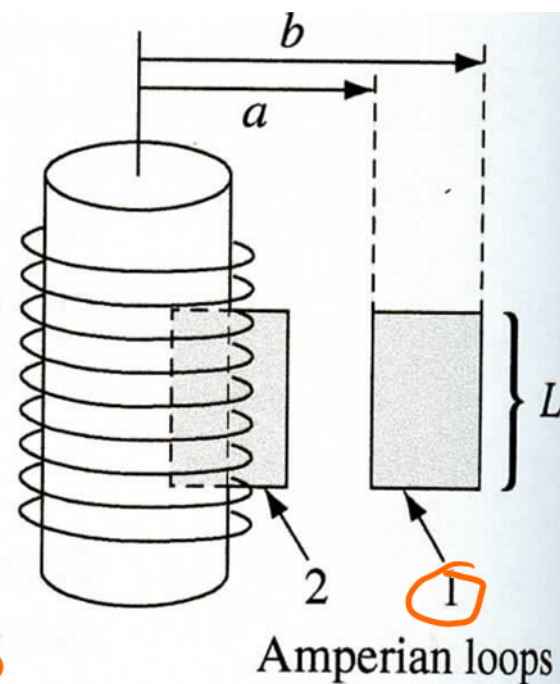
LOOP 1 - OUTSIDE SOLENOID

$$\oint \vec{B} \cdot d\vec{\ell} = [B(a) - B(b)] \cdot L = \mu_0 I_{enc}$$

SO  $B(a) = B(b)$

FIELD DOES NOT DEPEND ON  $s$ ,

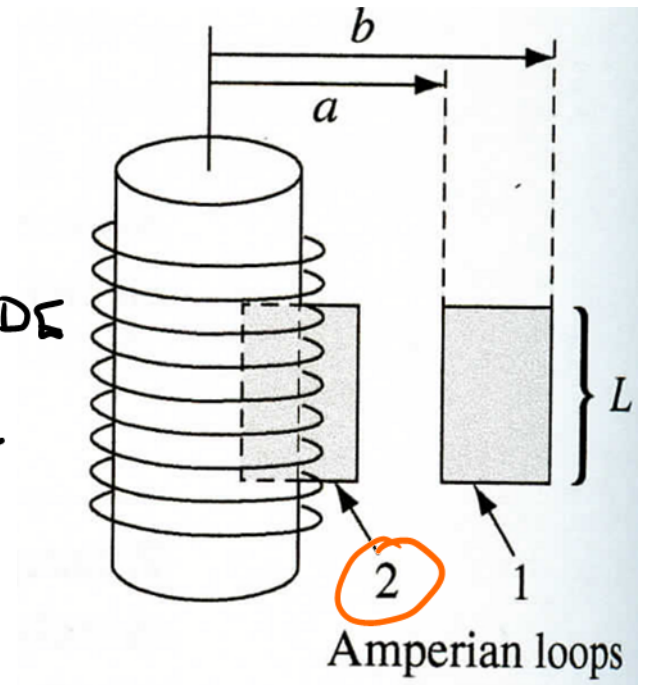
BUT  $s \rightarrow \infty \quad B \rightarrow 0 \Rightarrow B = 0$  EVERYWHERE



LOOP 2  $\rightarrow$   $\frac{1}{2}$  INSIDE,  $\frac{1}{2}$  OUTSIDE

AMPÈRE:

$$\begin{aligned}\int \vec{B} \cdot d\vec{\ell} &= B L_{\text{INSIDE}} + B L_{\text{OUTSIDE}} \\ &= \mu_0 I_{\text{enc}} + \mu_0 I_{\text{enc}} \\ &\quad \parallel \quad \parallel \\ &\quad n I L \quad 0 \\ &= \mu_0 n I L\end{aligned}$$



$$B = \begin{cases} \mu_0 I n \hat{z} & \text{INSIDE} \\ 0 & \text{OUTSIDE} \end{cases}$$

FIELD IS UNIFORM

MS  $\rightarrow$  SOLENOID

ES  $\rightarrow$   $\parallel^l$  PLATE CAPACITOR



AMPÈRE → ANALOG OF GAUSS IN ELECTROSTATICS

ALWAYS TRUE → ONLY USEFUL IF SYMMETRY ALLOWS

$$\oint \vec{B} \cdot d\vec{\ell} \rightarrow B \oint d\ell$$

— INFINITE STRAIGHT LINES

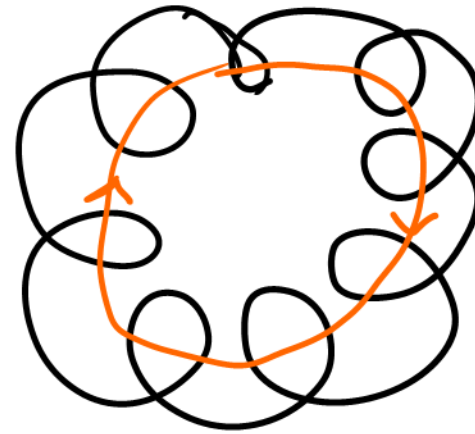
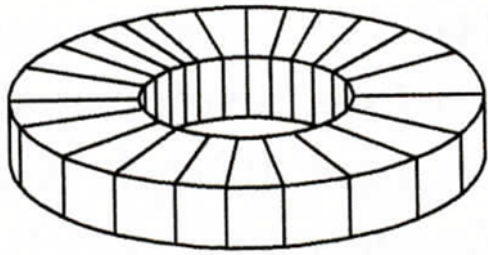
— INFINITE PLANES

— INFINITE SOLENOIDS

— TOROIDS

TOROID: A TOROIDAL COIL IS A CIRCULAR RING AROUND WHICH A LONG WIRE IS WRAPPED.

WINDING IS UNIFORM & TIGHT → EACH TURN IS A CLOSED LOOP  
SHAPE OF COIL DOESN'T MATTER



LOOKS LIKE A SOLENOID TURNED BACK ON ITSELF

↳ MAGNETIC FIELD IS CIRCUMFERENTIAL AT ALL POINTS INSIDE & OUTSIDE THE TOROID.

FIELD AT  $\vec{r}$  DUE TO ELEMENT  $\vec{r}'$

$$d\vec{B} = \frac{\mu_0}{4\pi} \frac{\vec{I} \times \vec{r}}{r^3} dl'$$

PUT  $\vec{r}$  IN  $xy$  PLANE

$$\vec{r} = (x, 0, z)$$

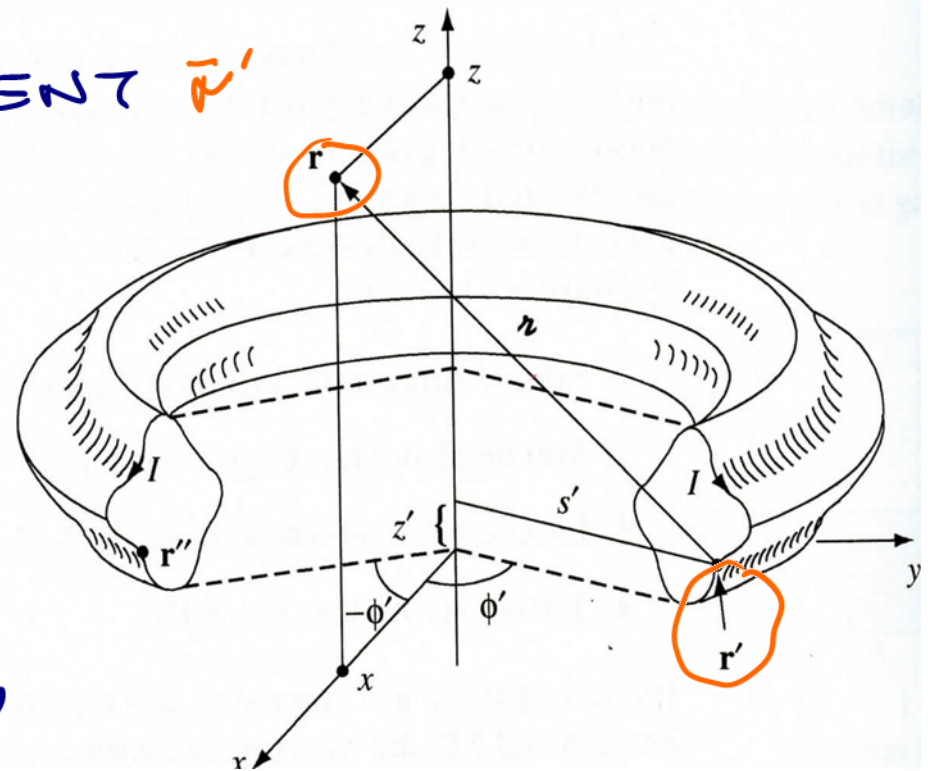
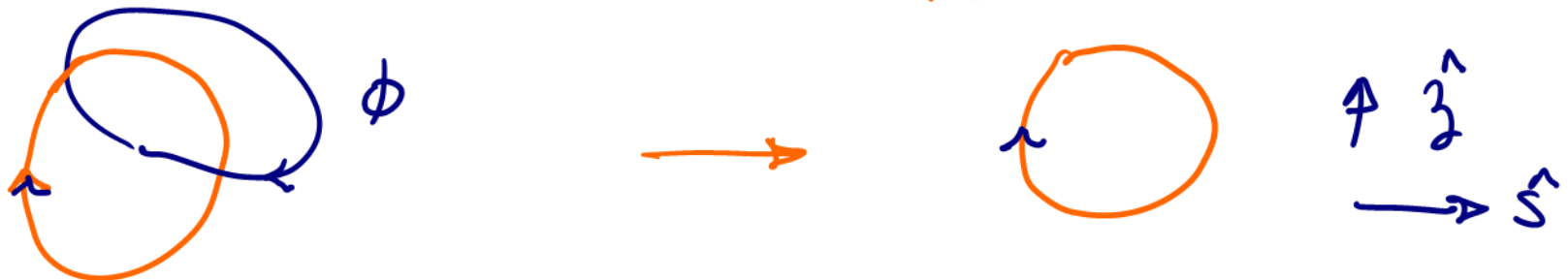
COORDINATES OF SOURCE  $\vec{r}'$

$$\vec{r}' = (s' \cos \phi', s' \sin \phi', z')$$

$$\vec{r} = (x - s' \cos \phi', -s' \sin \phi', z - z')$$

CURRENT HAS NO  $\phi$ -COMPONENT

ASSUME INDEPENDENT LOOPS



NO  $\phi$  COMPONENT

$$\vec{I} = I_s \hat{s} + I_z \hat{z} \quad \text{CYLINDRICAL}$$

IN CARTESIAN COORDS

$$\vec{I} = (I_s \cos \phi', I_s \sin \phi', I_z)$$

$$\vec{I} \times \vec{r} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ I_s \cos \phi' & I_s \sin \phi' & I_z \\ (x - s' \cos \phi') & (-s' \sin \phi') & (z - z') \end{vmatrix}$$

$$= \hat{x} \begin{vmatrix} I_s \sin \phi' & I_z \\ -s' \sin \phi' & z - z' \end{vmatrix} - \hat{y} \begin{vmatrix} I_s \cos \phi' & I_z \\ x - s' \cos \phi' & z - z' \end{vmatrix} + \hat{z} \begin{vmatrix} I_s \cos \phi' & I_s \sin \phi' \\ x - s' \cos \phi' & -s' \sin \phi' \end{vmatrix}$$

$$= \hat{x} (I_s \sin \phi' (z - z') + I_z s' \sin \phi')$$

$$- \hat{y} (I_s \cos \phi' (z - z') - I_z (x - s' \cos \phi'))$$

$$+ \hat{z} (I_s \cos \phi' (-s' \sin \phi') - I_s \sin \phi' (x - s' \cos \phi'))$$

$$= \hat{x} ( \sin \phi' (I_s (z - z')) + s' I_z )$$

$$+ \hat{y} ( I_z (x - s' \cos \phi') - I_s \cos \phi' (z - z') )$$

$$+ \hat{z} ( - I_s \cos \phi' \cdot s' \sin \phi' + I_s \sin \phi' \cdot s' \cos \phi' - I_s x \cdot \sin \phi' )$$

$$= [ \sin \phi' ( I_s (z - z') + s' I_z ) ] \hat{x}$$

$$+ [ I_z (x - s' \cos \phi') - I_s \cos \phi' (z - z') ] \hat{y}$$

$$+ [ - I_s x \sin \phi' ] \hat{z}$$

SYMMETRICAL ELEMENTS  $\bar{P}' \leftrightarrow \bar{P}''$

SAME  $s'$ ,  $r$ ,  $dl'$ ,  $I_s$ ,  $I_z$ ,  $\phi'$  -ve

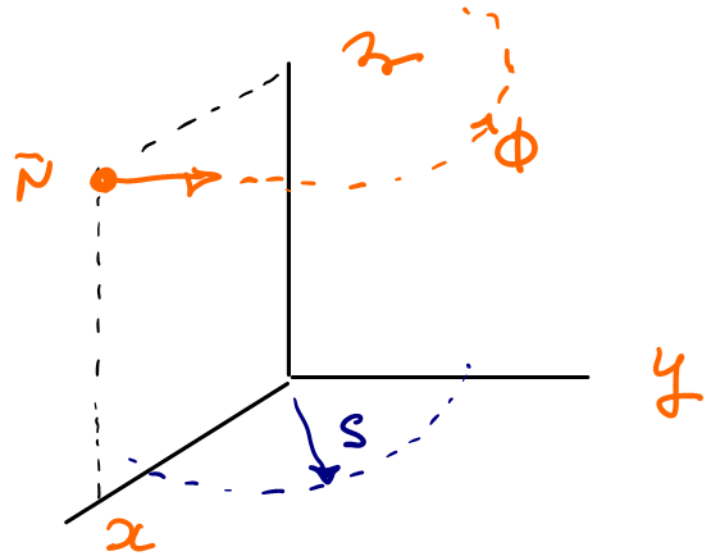
$\sin \phi' \rightarrow -\sin \phi'$  \* THESE TERMS CANCEL

ONLY HAVE  $\hat{y}$  TERM

SINCE PUT  $\vec{r}$  ON  $(x-z)$  PLANE

$\vec{r}$  POINTS IN  $y$ -DIRECTION

SO, IN GENERAL FIELD  $\hat{\phi}$

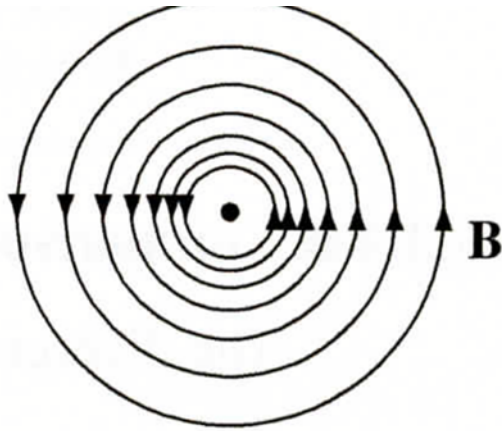


APPLY AMPÈRE'S LAW TO CIRCLE RADIUS  $s$

$$B 2\pi s = \mu_0 I_{enc} \rightarrow NI \rightarrow \text{TOTAL NUMBER OF TURNS}$$

$$\vec{B}(\vec{r}) = \begin{cases} \frac{\mu_0 NI}{2\pi s} \hat{\phi} & \text{INSIDE TOROID} \\ \vec{0} & \text{OUTSIDE TOROID} \end{cases}$$

# MAGNETOSTATICS ↔ ELECTROSTATICS



LONG WIRE

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J} \quad \text{AMPÈRE}$$

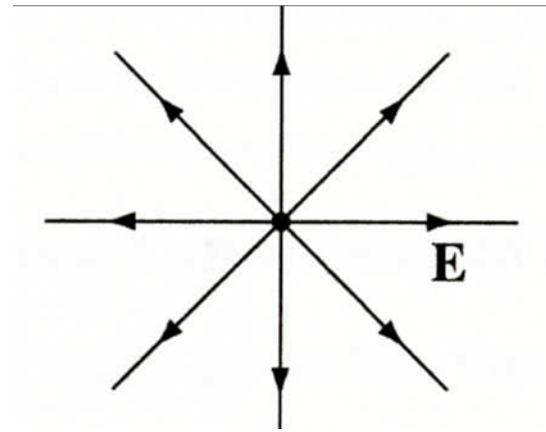
WITH  $\vec{B} \rightarrow 0$  @  $\infty$

DETERMINE  $\vec{B}$  from  $\vec{J}$

BIOT-SAVARD

+

SUPERPOSITION



POINT CHARGE

$$\vec{\nabla} \cdot \vec{E} = \rho / \epsilon_0 \quad \text{GAUSS}$$

$$\vec{\nabla} \times \vec{E} = \vec{0}$$

WITH  $\vec{E} \rightarrow 0$  @  $\infty$

DETERMINE  $\vec{E}$  from  $\rho$

Coulomb + SUPERPOSITION

MAXWELL'S STATIC EQUATIONS

$$\vec{\nabla} \cdot \vec{E} = \rho / \epsilon_0$$

$$\vec{\nabla} \times \vec{E} = \vec{0}$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

$$\vec{F} = q (\vec{E} + \vec{v} \times \vec{B})$$

CONCISE FORMULATION  
of  
ELECTROSTATICS  
MAGNETOSTATICS

- $\vec{E}$  DIVERGES FROM CHARGE
- $\vec{B}$  CURLS AROUND CURRENT
- $\vec{E}$  LINES START & END ON CHARGES
- $\vec{B}$  LINES CLOSED LOOPS OR  $\rightarrow \infty$ 
  - $\hookrightarrow \vec{\nabla} \cdot \vec{B} = 0$
  - $\hookrightarrow$  NO MAGNETIC CHARGES

GENERALLY

$$\vec{E} \gg \vec{B}$$

$\hookrightarrow$  CAN MAKE LARGE  $F$  FROM  
LARGE CURRENTS

$\vec{E} \sim 0 \rightarrow$  WIRES NEUTRAL