

MAGNETIC VECTOR POTENTIAL

FROM $\vec{\nabla} \times \vec{E} = \vec{0} \rightarrow \vec{E} = -\vec{\nabla} V$ SCALAR POTENTIAL

FROM $\vec{\nabla} \cdot \vec{B} = 0 \rightarrow \vec{B} = \vec{\nabla} \times \vec{A}$ VECTOR POTENTIAL

THIS AUTOMATICALLY $\vec{\nabla} \cdot \vec{B} = 0$

$$\vec{\nabla} \cdot (\vec{\nabla} \times \vec{A}) = 0$$

AMPÈRE'S LAW

$$\vec{\nabla} \times \vec{B} = \vec{\nabla} \times (\vec{\nabla} \times \vec{A}) = \underbrace{\vec{\nabla}(\vec{\nabla} \cdot \vec{A}) - \nabla^2 \vec{A}}_{\text{LOOKS COMPLICATED}} = \mu_0 \vec{J}$$

LOOKS COMPLICATED

RECALL \rightarrow CAN ADD ANY F , $\vec{\nabla} F = 0$ TO V

CAN ADD TO \vec{A} ANY \vec{F} , $\vec{\nabla} \times \vec{F} = 0$ GRADIENT OF ANY SCALAR

\rightarrow MAKE $\vec{\nabla} \cdot \vec{A} = 0$

SUPPOSE \vec{A}_0 NOT DIVERGENCELESS

ADD GRADIENT of $\lambda \rightarrow \vec{A} = \vec{A}_0 + \vec{\nabla}\lambda$

NEW DIVERGENCE

$$\vec{\nabla} \cdot \vec{A} = \vec{\nabla} \cdot \vec{A}_0 + \nabla^2 \lambda$$

CAN MAKE $\vec{\nabla} \cdot \vec{A} \rightarrow 0$ IF $\nabla^2 \lambda = -\vec{\nabla} \cdot \vec{A}_0$

KNOW HOW TO SOLVE \rightarrow THIS IS JUST POISSON

$$\nabla^2 V = -\frac{\rho}{\epsilon_0}$$

$$V = \frac{1}{4\pi\epsilon_0} \int \frac{\rho}{r} dz'$$

$$\lambda = \frac{1}{4\pi} \int \frac{\vec{\nabla} \cdot \vec{A}_0}{r} dz'$$

IF $\rho \rightarrow 0 @ \infty$

IF $\vec{\nabla} \cdot \vec{A}_0 \rightarrow 0 @ \infty$

ALWAYS POSSIBLE $\vec{\nabla} \cdot \vec{A} \rightarrow 0$
TO MAKE

CAN ALWAYS MAKE $\vec{\nabla} \cdot \vec{A} \rightarrow 0$

THE DEFINITION $\vec{B} = \vec{\nabla} \times \vec{A}$ SAYS NOTHING ABOUT

$\vec{\nabla} \cdot \vec{A}$
CHOOSE 0 \rightarrow CAN CHOOSE IT
ANYWAY WE LIKE

$$\vec{\nabla} \times \vec{B} = \vec{\nabla} \times (\vec{\nabla} \times \vec{A}) = \vec{\nabla}(\vec{\nabla} \cdot \vec{A}) - \nabla^2 \vec{A} = \mu_0 \vec{J}$$

BECOMES $\nabla^2 \vec{A} = -\mu_0 \vec{J} \leftarrow$ AMPÈRE'S
LAW
 \rightarrow POISSON 3-d LAW

WE KNOW THE SOLUTION IS

$$\vec{A}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{J}(\vec{r}')}{r} d\tau'$$

ASSUME $\vec{J} \rightarrow 0$
 $\odot \infty$

LINE CURRENT $\vec{A} = \frac{\mu_0}{4\pi} \int \frac{\vec{I}}{r} dl' = \frac{\mu_0 I}{4\pi} \int \frac{1}{r} dl'$

SURFACE CURRENT $\vec{A} = \frac{\mu_0}{4\pi} \int \frac{\vec{K}}{r} da'$

\vec{A} NOT AS USEFUL AS $V \rightarrow$ IT'S A VECTOR

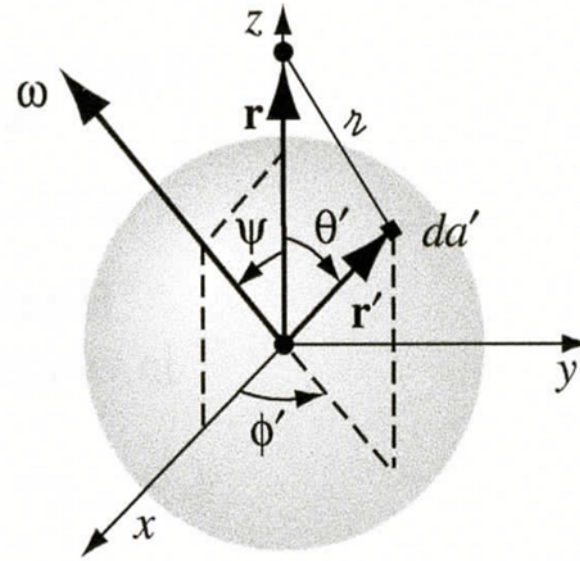
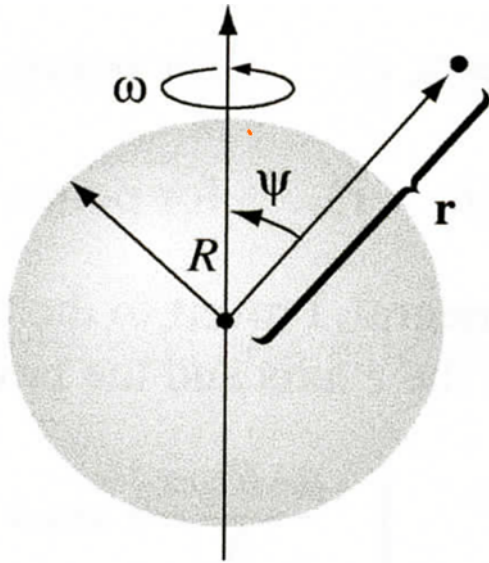
WOULD BE NICE IF $\vec{B} = -\vec{\nabla} u$ SCALAR

THIS CONTRADICTS $\nabla^2 \vec{A} = -\mu_0 \vec{J} \rightarrow \vec{\nabla} \times (\vec{\nabla} u) = 0$

SINCE MAGNETIC FORCES DO NO WORK

\vec{A} CAN NOT BE INTERPRETED SIMPLY
AS POTENTIAL ENERGY / UNIT CHARGE

EXAMPLE: SPHERICAL SHELL RADIUS R UNIFORM SURFACE CHARGE σ SPINNING AT ANGULAR VELOCITY ω . FIND VECTOR POTENTIAL AT A POINT r



PUT r ALONG z -AXIS, ω TILTED AT ANGLE ϕ
 ω LIES IN xz PLANE

$$A(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{K}(\vec{r}')}{r} da'$$

SURFACE CURRENT

$$A(\vec{r}) = \frac{M_0}{4\pi} \int \frac{\vec{K}(\vec{r}')}{r} da'$$

$$\vec{K} = \sigma \vec{v} \text{ VELOCITY} \quad r = (R^2 + r'^2 - 2Rr' \cos\theta')^{\frac{1}{2}}$$

$$da' = R^2 \sin\theta' d\theta' d\phi'$$

LAW OF COSINES $\vec{r} = \vec{r}' - R$

$$r^2 = (\vec{r}' - R)^2$$

$$r^2 = (r'^2 + R^2 - 2Rr' \cos\theta')$$

VELOCITY OF POINT \vec{r}' ON ROTATING RIGID BODY

$$\vec{v} = \vec{\omega} \times \vec{r}'$$

$\vec{\omega}$ IS IN XY PLANE

GENERALLY - SPHERICAL COOR DS

$$\omega_z = \omega \cos\psi$$

$$x = r \sin\theta \cos\phi, y = r \sin\theta \sin\phi, z = r \cos\theta$$

$$\omega_x = \omega \sin\psi$$

$$x = R' \sin\theta' \cos\phi', y = R' \sin\theta' \sin\phi', z = R' \cos\theta'$$

$$\omega_y = 0$$

$$\vec{V} = \vec{\omega} \times \vec{r} \quad \left| \begin{array}{ccc} \hat{x} & \hat{y} & \hat{z} \\ \omega \sin \psi & 0 & \omega \cos \psi \\ R \sin \theta' \cos \phi' & R \sin \theta' \sin \phi' & R \cos \theta' \end{array} \right|$$

$$= R\omega \left(-\cancel{\cos \psi \sin \theta' \sin \phi'} \right) \hat{x} + R\omega \left(\cancel{\cos \psi \sin \theta' \cos \phi'} - \sin \psi \cos \theta' \right) \hat{y} - R\omega \left(\cancel{\cos \psi \sin \theta' \sin \phi'} \right) \hat{z}$$

$$\int_0^{2\pi} \sin \phi' d\phi' = 0 \quad ; \quad \int_0^{2\pi} \cos \phi' d\phi' = 0$$

TERMS IN $\sin \phi'$, $\cos \phi' \rightarrow 0$

$$\vec{V} = -R\omega \sin \psi \cos \theta' \hat{y}$$

$$\vec{A}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{K}}{r} d\tau = \hat{y} \frac{\mu_0}{4\pi} \int \frac{-R\omega \sin \psi \cos \theta' r^2 \sin \theta' dr d\theta' d\phi'}{(R^2 + r^2 - 2Rr \cos \theta')} \quad \text{CONSTANT}$$

NO INTEGRAL OVER r
 $r \rightarrow R$

$$\bar{A}(F) = \frac{-\mu_0}{4\pi} R \sigma \omega \sin^4 \theta \int_0^{2\pi} d\phi' \int_0^\pi \frac{R^2 \cos\theta' \sin\theta' d\theta'}{(\dots)^{\frac{1}{2}}}$$

$$= \frac{-\mu_0}{2} R^3 \sigma \omega \sin^4 \theta \int_0^\pi \frac{\cos\theta' \sin\theta' d\theta'}{(\dots)^{\frac{1}{2}}}$$

PUT $u = \cos\theta'$, $du = -\sin\theta' d\theta'$

HAVE $\int_{-1}^{+1} \frac{u du}{(R^2 + r^2 - 2ru)}$

KNOW THAT $\int \frac{x dx}{(a+bx)^{\frac{1}{2}}} = \frac{-2(2a-bx)}{3b^2} \sqrt{a+bx}$

$a = R^2 + r^2$, $b = -2Rr$

$$\int = \frac{-2(2R^2 + 2r^2 + 2Rru)}{3(-2Rr)^2} \sqrt{\dots}$$

$$\int_{-1}^{+1} \rightarrow \frac{- (R^2 + r^2 + Rr u)}{3R^2 r^2} \sqrt{\dots}$$

$$\text{FOR } u = +1 = \frac{-1}{3R^2 r^2} (R^2 + r^2 + Rr)(R - r)$$

$$u = -1 = \frac{-1}{3R^2 r^2} (R^2 + r^2 - Rr) (R^2 + r^2 + 2Rr)^{\frac{1}{2}}$$

$$= \frac{1}{3R^2 r^2} (R^2 + r^2 - Rr)(R + r)$$

HAVE TO TAKE +VE $\sqrt{\quad}$ IN EACH CASE

$$\vec{A}(\vec{r}) \begin{cases} \frac{\mu_0 R \sigma}{3} (\vec{\omega} \times \vec{r}) & \text{INSIDE SPHERE} \\ \frac{\mu_0 R^4 \sigma}{3r^2} (\vec{\omega} \times \vec{r}) & \text{OUT SIDE SPHERE} \end{cases}$$

$$\vec{\omega} \times \vec{r} = \omega r \sin \theta \quad \text{in } \hat{\phi} \text{ DIRECTION}$$

$$\vec{A}(r, \theta, \phi) = \begin{cases} \frac{\mu_0 R \omega \sigma}{3} r \sin \theta \hat{\phi} & r \leq R \\ \frac{\mu_0 R^4 \omega \sigma}{3} \frac{r}{r^3} \sin \theta \hat{\phi} & r \geq R \end{cases}$$

NOW USE \vec{A} TO GET \vec{B}

$$\begin{aligned} \vec{B} = \vec{\nabla} \times \vec{A} &= \frac{1}{r \sin \theta} \left[\frac{\partial}{\partial \theta} (r \sin \theta A_\phi) - \frac{\partial A_\theta}{\partial \phi} \right] \hat{r} \\ &+ \frac{1}{r} \left[\frac{1}{\sin \theta} \frac{\partial A_r}{\partial \phi} - \frac{\partial}{\partial r} (r A_\phi) \right] \hat{\theta} \\ &+ \frac{1}{r} \left[\frac{\partial}{\partial r} (r A_\theta) - \frac{\partial A_r}{\partial \theta} \right] \hat{\phi} \end{aligned}$$

$\vec{A} \rightarrow A_\phi \hat{\phi} \therefore$ ONLY A_ϕ TERMS CONTRIBUTE, $r \leq R$
INSIDE

$$\textcircled{1} \quad \frac{\mu_0 R \omega \sigma}{3} \left[\frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (r \sin^2 \theta) \right] \hat{r}$$

$$= \frac{\mu_0 R \omega \sigma}{3} \cdot \frac{2 \sin \theta \cos \theta r}{r \sin \theta} = \frac{\mu_0 R \omega \sigma}{3} \cdot 2 \cos \theta \hat{r}$$

$$\textcircled{2} \quad -\frac{\mu_0 R \omega \sigma}{3} \cdot \frac{1}{r} \frac{\partial}{\partial r} (r \cdot r \sin \theta) \hat{\phi} = -\frac{\mu_0 R \omega \sigma}{3} \frac{1}{r} 2r \sin \theta \hat{\phi}$$

$$\text{so } \nabla \times \vec{A} = \vec{B} = \frac{\mu_0 R \omega \sigma}{3} \left(\underbrace{2 \cos \theta \hat{r} - 2 \sin \theta \hat{\phi}}_{2 \hat{z}} \right)$$

$$\vec{B} = \frac{2 \mu_0 \sigma R \omega}{3} \hat{z}$$

$$\vec{B} = \frac{2}{3} \mu_0 \sigma R \omega \hat{z} \quad \leftarrow \text{UNIFORM INSIDE SPHERE}$$

EXAMPLE: FIND VECTOR POTENTIAL OF ∞ SOLENOID
 n TURNS PER UNIT LENGTH, RADIUS R
 CURRENT I .

CANNOT USE $\vec{A} = \frac{\mu_0}{4\pi} \int \frac{\vec{I}}{r} dl'$ CURRENT EXTENDS TO ∞

$$\textcircled{1} \oint \vec{A} \cdot d\vec{\ell} = \int (\vec{\nabla} \times \vec{A}) \cdot d\vec{a}' = \int \underbrace{\vec{B}}_{\vec{B} = \vec{\nabla} \times \vec{A}} \cdot d\vec{a} = \underline{\underline{\Phi}}$$

STOKES

$\underline{\underline{\Phi}}$ IS FLUX OF \vec{B} THRU ONE TURN LOOP

AMPÈRE'S LAW $\oint \vec{B} \cdot d\vec{\ell} = \mu_0 I_{enc}$ CURRENT ENCLOSED BY AMPER LOOP

THIS IS SAME AS $\textcircled{1}$ ABOVE WITH

$$\vec{B} \rightarrow \vec{A}$$

$$\mu_0 I_{enc} \rightarrow \underline{\underline{\Phi}}$$

IN SYMMETRICAL SITUATION CAN DETERMINE

\vec{A} from $\vec{\mathcal{O}}$

JUST AS \vec{B} from I_{encl}

WE HAVE UNIFORM LONGITUDINAL MAGNETIC FIELD
INSIDE SOLENOID, NO FIELD OUTSIDE

ANALAGOUS TO AMPERE LAW TO SOLVE THICK WIRE
CARRYING UNIFORM CURRENT

- VECTOR POTENTIAL $\oint_{\vec{a}} \vec{A}$ \leftrightarrow $\oint_{\vec{a}} \vec{B}$

USE CIRCULAR AMPERIAN LOOP RADIUS S INSIDE SOLENOID

$$\oint \vec{A} \cdot d\vec{e} = A \cdot 2\pi S = \int \vec{B} \cdot d\vec{a}$$

\int AROUND LOOP $\vec{B} = \mu_0 n I$ πS^2

$$\int \vec{B} \cdot d\vec{a} = \mu_0 n I \pi s^2$$

$$\vec{A} = \frac{\mu_0 n I s}{2} \hat{\phi} \quad \text{for } s \leq R$$

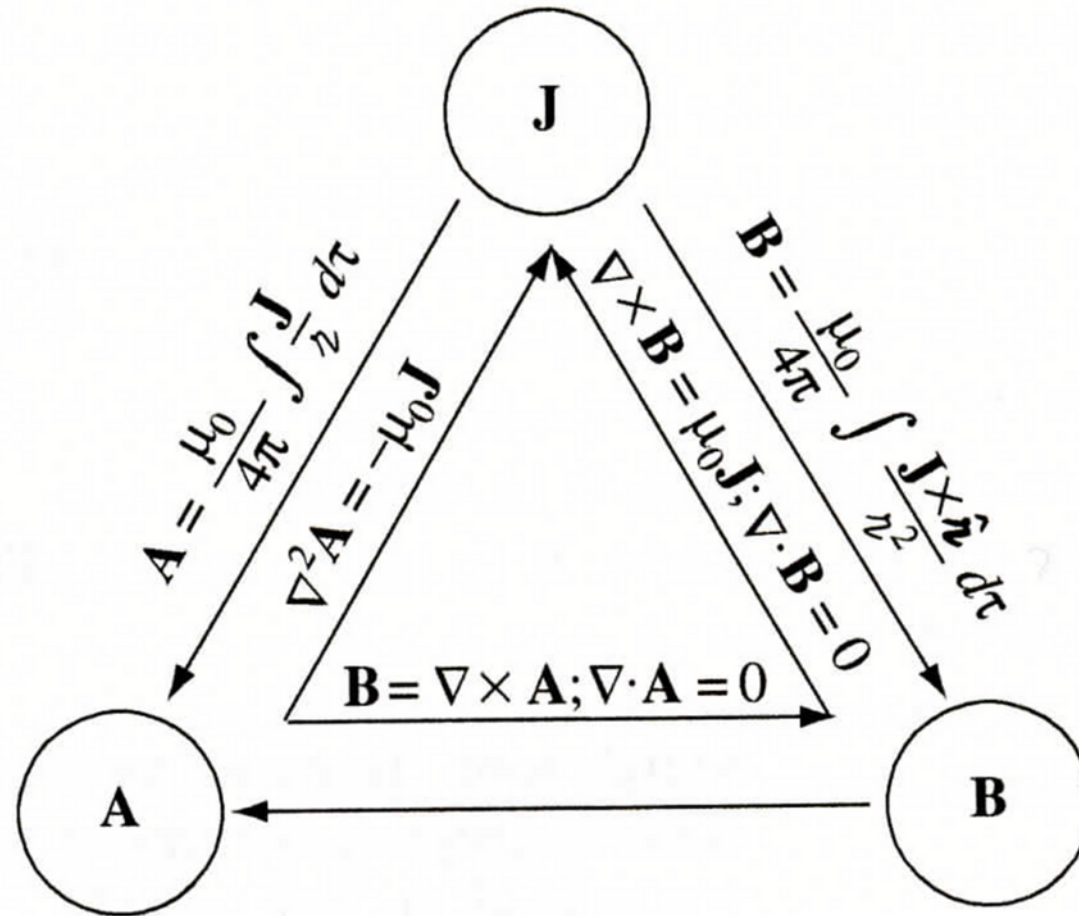
\vec{B} IS ZERO OUTSIDE SOLENOID

SO MAXIMUM AMPERIAN LOOP \rightarrow RADIUS R

$$\int \vec{B} \cdot d\vec{a} = \underbrace{\mu_0 n I}_{\text{AREA OF AMPERIAN LOOP}} \cdot \underbrace{\pi R^2}_{\text{AREA OF AMPERIAN LOOP}}$$

$$\vec{A} = \frac{\mu_0 n I}{2} \cdot \frac{R^2}{s} \hat{\phi} \quad \text{for } s \geq R$$

TRIANGLE SUMMARY of MAGNETOSTATICS



BOUNDARY CONDITIONS

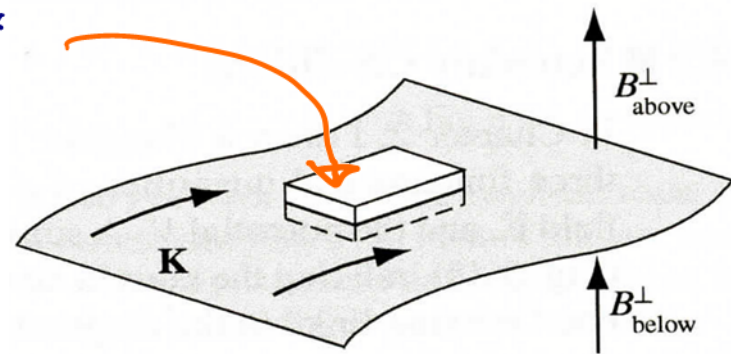
ELECTROSTATICS $\rightarrow \vec{E}$ DISCONTINUOUS @ SURFACE CHARGE

MAGNETOSTATICS $\rightarrow \vec{B}$ DISCONTINUOUS @ SURFACE CURRENT

\hookrightarrow TANGENTIAL COMPONENT CHANGES

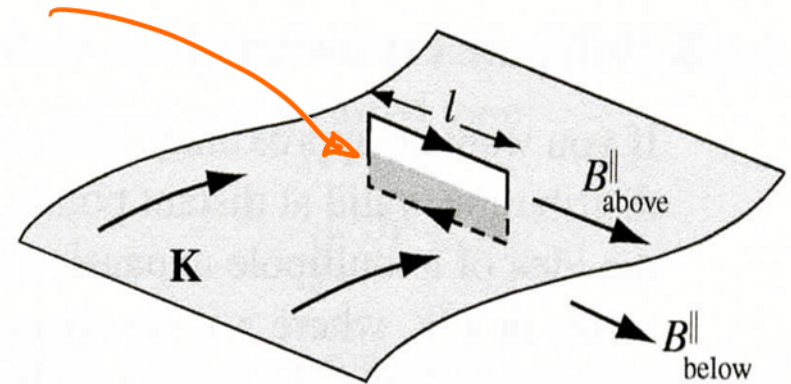
APPLY $\oint \vec{B} \cdot d\vec{a} = 0$ TO ALL BOX

$$B_{\text{ABOVE}}^{\perp} = B_{\text{BELOW}}^{\perp}$$



AMPERIAN LOOP PERP TO CURRENT

$$\begin{aligned} \oint \vec{B} \cdot d\vec{l} &= (B_{\text{ABOVE}}^{\parallel} - B_{\text{BELOW}}^{\parallel}) l \\ &= \mu_0 I_{\text{enc}} = \mu_0 K l \end{aligned}$$

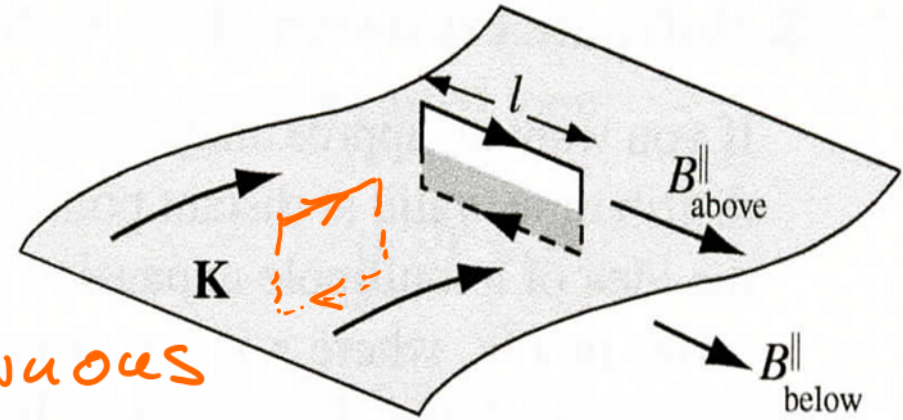


$$B_{\text{ABOVE}}^{\parallel} - B_{\text{BELOW}}^{\parallel} = \mu_0 K$$

AMPERIAN LOOP \parallel TO CURRENT

\vec{B} PARALLEL TO LOOP IS
SAME ON EACH SIDE OF LOOP

SO \vec{B} PARALLEL TO CURRENT CONTINUOUS



SUMMARIZE AS: $\vec{B}_{\text{ABOVE}} - \vec{B}_{\text{BELOW}} = \mu_0 (\vec{K} \times \hat{n})$

LIKE SCALAR \vec{E} POTENTIAL, \vec{A} CONTINUOUS OVER
BOUNDARY

$$\vec{A}_{\text{ABOVE}} = \vec{A}_{\text{BELOW}}$$

$\vec{\nabla} \cdot \vec{A} = 0 \Rightarrow$ IMPLIES NORMAL

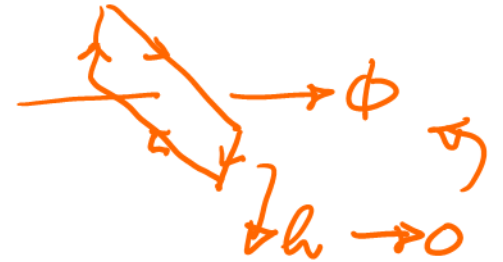
COMPONENT CONTINUOUS

$$\left. \begin{array}{c} \uparrow A \\ \hline \uparrow \vec{A} \end{array} \right\} \vec{\nabla} \cdot \vec{A} = 0$$

USED STOKES TO SHOW THAT

$$\oint \vec{A} \cdot d\vec{e} = \int \vec{B} \cdot d\vec{a} = \underline{\underline{\Phi}} \quad \leftarrow \text{FLUX THRU LOOP}$$

LOOP OF ZERO THICKNESS $\underline{\underline{\Phi}} \rightarrow 0$



$$\vec{B}_{\text{ABOVE}} - \vec{B}_{\text{BELOW}} = \mu_0 \vec{K} \times \hat{n}$$

$$\vec{\nabla} \times \vec{A}_{\text{ABOVE}} - \vec{\nabla} \times \vec{A}_{\text{BELOW}} = \mu_0 \vec{K} \times \hat{n} \quad \leftarrow \text{DISCONTINUOUS}$$

$$\frac{\partial \vec{A}_{\text{ABOVE}}}{\partial n} - \frac{\partial \vec{A}_{\text{BELOW}}}{\partial n} = \mu_0 \vec{K}$$